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Fiberglass Composite Repairs Presentation

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Fiberglass Composite Repairs

Brad Fenbert, along with Ian Saksa Project Adviser: Dr. Tanveer Chawla



Composite Overview

 A composite is a material with a matrix (resin) and reinforcement (fibers)

Concrete/rebar, wood (cellulose fibers and lignin),

carbon fiber/epoxy

 Used in a variety of fields: airplanes, boats, wind turbine blades, sports equipment

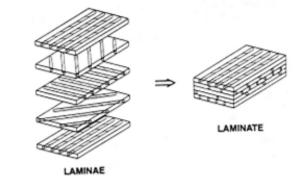


Figure 1. Laminate Composite [1]



Composite Repairs

Repairs are a necessary part of composite life cycle

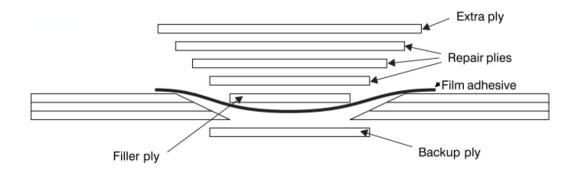


Figure 2. Taper sanded (scarf) repair [2]



Project Overview

Problem: Determination of fiberglass composite repair factors that affect crack propagation fracture toughness.

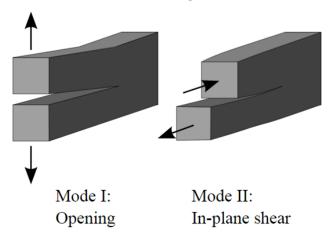


Figure 3. Crack Propagation Modes [3]



Project Objectives

- Factors must have an expected affect on crack propagation fracture toughness
- The testing and manufacturing procedure should be repeatable
- The testing apparatus and equipment must be able to effectively monitor crack growth
- The testing procedure should replicate conditions the repairs will experience in use
- The materials and equipment used will be those that are available from the PET lab
- The cost for materials and equipment required for the study should be minimized
- Wear on lab equipment should be minimized



Project Design

- Factors: resin, grinding depth, and chopped strand mat
- Testing under ASTM D6671 Mixed Mode Testing
- Three mode mixture ratios, 5 specimens each, total of 120 specimens
- Total mixed-mode fracture toughness (G_C) would be calculated

Table 1. 2³ Factorial Design

Run#	Coded Factor Levels			Uncoded		
Kull #		oueu raci	or Levels	Grind depth	Resin	Chopped Strand Mat
1	-	-	-	half	Polyester	No CSM
2	-	-	+	half	Polyester	CSM
3	-	+	-	half	Vinylester	No CSM
4	-	+	+	half	Vinylester	CSM
5	+	-	-	full	Polyester	No CSM
6	+	-	+	full	Polyester	CSM
7	+	+	-	full	Vinylester	No CSM
8	+	+	+	full	Vinylester	CSM



Parent Plates

Plates were manufactured using Vacuum Assisted Resin Transfer Method

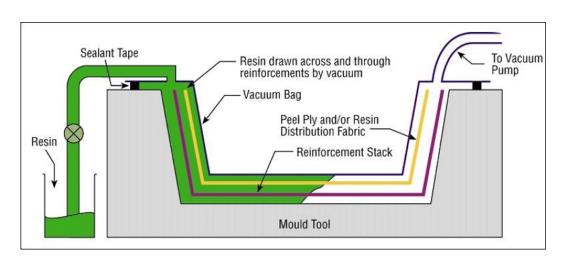


Figure 4. VARTM Diagram [4]



Figure 5. VARTM Setup



Grinding



Figure 6. Grinding Setup

- Table frequently got stuck
- Grind depth would surpass router setting
- Table deflected in the middle
- Table accommodated 15.75" plates
- Relied on visual cues





Figure 7. Full (left) vs half grind (right) surfaces



Hand Lay up

- Clean surface of plate with stiff resin brush
- Place 7.5cm crack initiation insert 7.5cm from edge
- polyester general purpose orthophthalic resin from jabberwocky composites IIc (B and J fiberglass)
- vinyl ester hydrex 100 from fiberglass supply



Figure 8. Cleaning plate surface

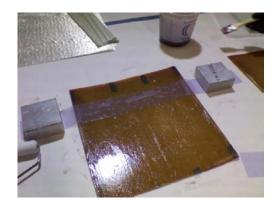


Figure 9. Crack Initiation Insert



Hand Lay up

- Place chopped strand mat
- Five 16x16" uni-directional fiberglass sheet
- One triaxial fiberglass on top
- Cure for 24 hours, post cure for 16 hours at 40 °C



Figure 10. Foam roller for resin



Figure 11. Metal roller for smoothing sheets



Specimen Preparation



Figure 12. Cutting out specimens

- Table saw did not cut straight, laser alignment was off
- Difficult to cut hinges straight



Figure 13. Cutting out hinges



Specimen Preparation

- Hinges were grinded, and teflon tape was added to allow consistent/even adhesive bonding surface
- Specimens were marked with white out and marked with fine tip ink pen marks to aid crack propagation/displacement measuring
- Hinges were adhered with methacrylate adhesive (Plexus MA300)

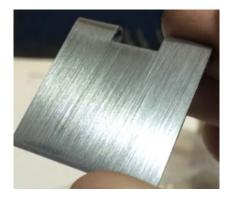


Figure 14. Roughed hinge surface



Figure 15. Teflon tape on hinges



Figure 16. Hinge held by clamp



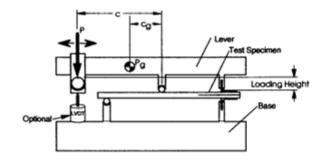


Figure 17. MMB testing apparatus [5]

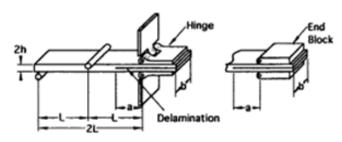


Figure 18. Specimen variables [5]

$$c = \frac{12\beta^{2} + 3\alpha + 8\beta\sqrt{3\alpha}}{36\beta^{2} - 3\alpha}L \qquad \alpha = \frac{1 - \frac{G_{II}}{G}}{\frac{G_{II}}{G}} \qquad \beta = \frac{\alpha + \chi h}{\alpha + 0.42\chi h}$$

$$\chi \equiv \sqrt{\frac{E_{11}}{11G_{13}}} \left\{ 3 - 2\left(\frac{\Gamma}{1 + \Gamma}\right)^{2} \right\} \qquad \Gamma = 1.18 \frac{\sqrt{E_{11}E_{22}}}{G_{13}}$$

$$E_{1f} = \frac{8(a_{0} + \chi h)^{3}(3c - L)^{2} + \left[6(a_{0} + 0.42\chi h)^{3} + 4L^{3}\right](c + L)^{2}}{16L^{2}bh^{3}\left(\frac{1}{m} - C_{sys}\right)}$$

$$G_{I} = \frac{12P^{2}(3c - L)^{2}}{16b^{2}h^{3}L^{2}E_{1f}}(\alpha + \chi h)^{2} \qquad G_{II} = \frac{9P^{2}(c + L)^{2}}{16b^{2}h^{3}L^{2}E_{1f}}(\alpha + 0.42\chi h)^{2}$$

$$G = G_{I} + G_{II} \qquad \frac{G_{II}}{G} = \frac{G_{II}}{G_{I} + G_{II}}$$

Figure 18. Calculation equations [5]



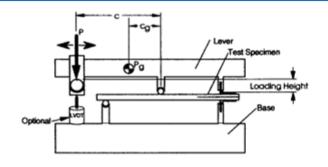


Figure 17. MMB testing apparatus [5]

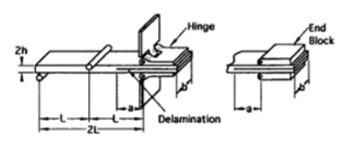


Figure 18. Specimen variables [5]

Variables recorded during testing:

a (mm): delamination length

P (Newtons): applied load

d (mm): opening displacement

Other variables:

b (mm): specimen width

h (mm): specimen half thickness

d (mm): opening displacement

m (N/mm): slope of load displacement curve

L (mm): half span length

C (mm): lever length



- Dinocapture 2.0 software with Dino-Lite Edge Digital usb microscope to capture crack propagation
- Vicsnap/Vic2d software with digital camera used to capture opening displacement
- Applied load measured with MTS Sintech 5/GL Testworks 4 software

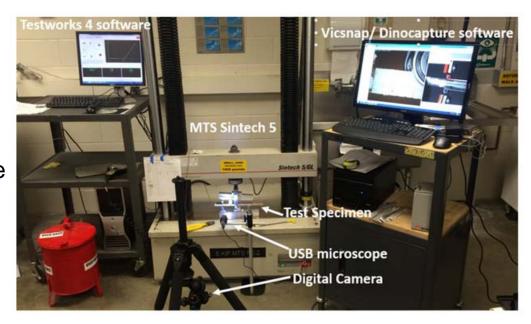


Figure 19. Testing setup





Figure 20. Load point deflection



Figure 21. Crack length

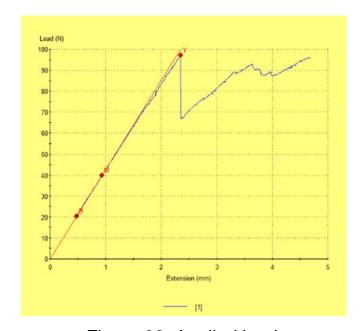


Figure 22. Applied load



Calculating variable m

- Digital camera was set to record one image every .5 seconds
- MTS measured applied load every half second

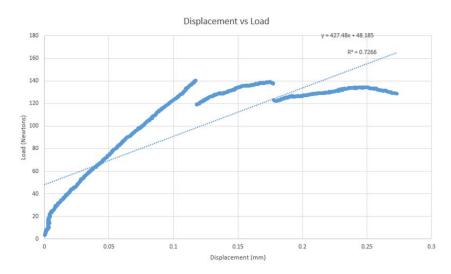


Figure 23. Raw load vs displacement data

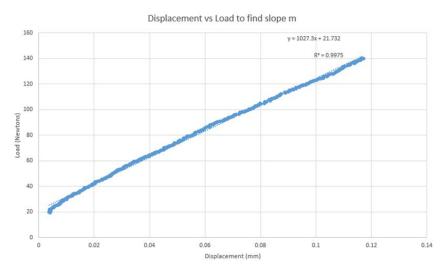


Figure 24. Refocused graph to determine slope of linear region (N/mm)



Calculating Crack Propagation & Loads

- Import MTS Data
- Sync Video & Load
- Record loads & corresponding crack propagations

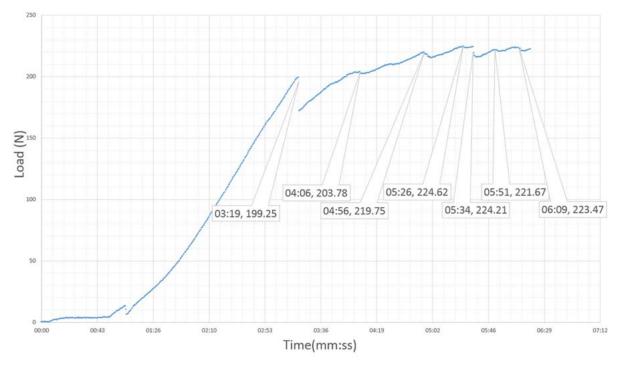


Figure 25. Load vs time graph



Results

- Only significant results were obtained with .2 Mode Mixture (High mode 1 -Tensile Load)
- Specimens at .5 and .8 either broke the hinges before the crack propagated, or propagated too quickly



Figure 26. Hinge right before breaking

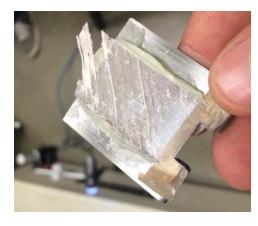


Figure 27. Broken Hinge



Results Overview

Table 2. Specimen Average Gc (Fracture Toughness) Value at .2 Mode Mixture*

Factor	Gc	%Increase	
Full Grind	7.728	∃ 31% ∣	
Half Grind	10.126		
Polyester	7.604	1 250/	
Vinyl Ester	10.253		
No CSM	6.515	1 74%	
CSM	11.344		

^{*}Values have been normalized.



Analysis - Grinding

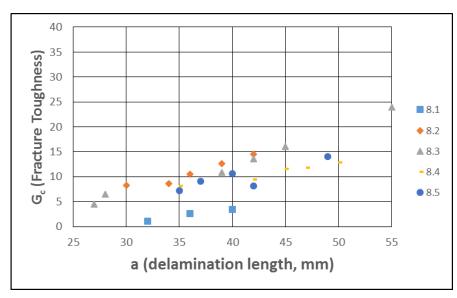


Figure 28. Plate 8 (full grind, csm, vinyl ester)*

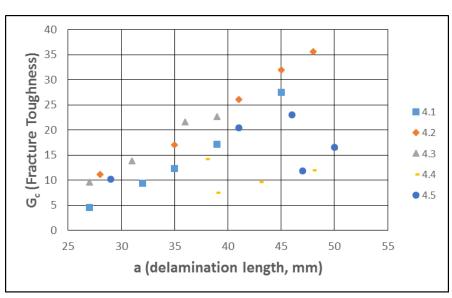


Figure 29. Plate 4 (1/2 grind, csm, vinyl ester)*

^{*}Values have been normalized.



Analysis - Resin

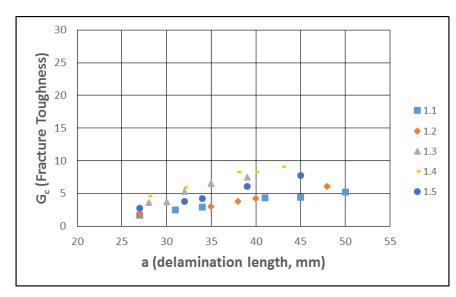


Figure 30. Plate 1 (1/2 grind, polyester, no csm)*

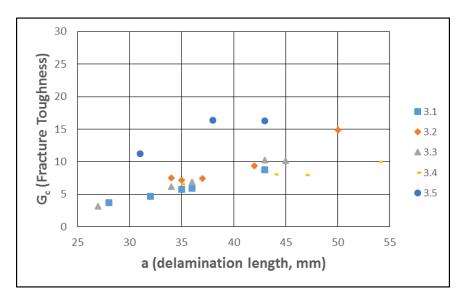


Figure 31. Plate 3 (1/2 grind, vinylester, no csm)*

^{*}Values have been normalized.



Analysis - Chopped Strand Mat

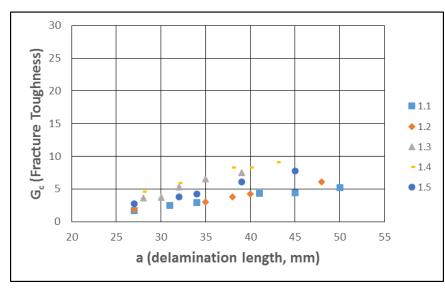


Figure 32. Plate 1 (½ grind, polyester, **no csm**)*

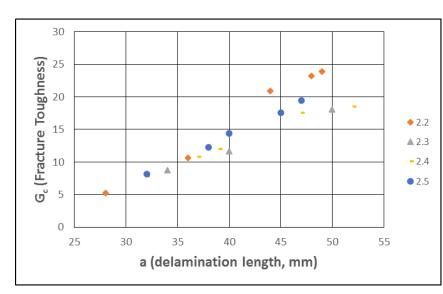


Figure 33. Plate 2 (½ grind, polyester, csm)*

^{*}Values have been normalized.

Reason for Results

Factors increased the amount of fiber bridging





Figure 34. Fiber bridging in Plate 5 (full grind, polyester) vs Plate 3 (½ grind, vinyl ester)



Future Recommendations

Plate manufacturing

Less thick specimens, in order to test modes .5 and .8 without breaking specimen hinge

Grinding

More consistent process, change apparatus so it doesn't deflect

Hinges

- Less teflon tape, although allowed smoother adhesion, didn't provide bond strength in critical area at load point, where hinges failed
- Stronger hinge adhesion, either resin or surface preparation of specimens

Specimen Prep

- Straighter cutting device, such as the water jet
- Wider specimens, help improve bonding surface area between hinges and specimens
- Less white out, make sure it does not flake
- More speckles at load point to allow for easier Vic 2d analysis



Future Recommendations

Testing

- Use calibration with mts to measure displacement, more consistent strategy and a lot less time consuming than vic 2d analysis
- Better way to sync different measurements systems
- Take pictures rather than video of crack propagation

Analysis

Use a better video playback software



Conclusion

Shortfallings

- Used more materials than expected exceeded budget estimate
- Were not able to collect significant data on Mode Mixtures .5 and .8

Successes

- Equipment used was able to effectively monitor crack growth
- All factors chosen had significant results in Mode Mixture .2, with the use of a chopped strand mat being the most prominent
- No damaged tools/lab equipment



Acknowledgements

I would like to thank Michael Airoldi and David Frye for their consistent help while working in the plastics labs.

This project could not have been completed without the guidance of my sponsor Tanveer Chawla.

References

- [1] FAO. "Composites." Application of Natural Fibre Composites in the Development of Rural Societies. N.p., 2015. Web. 12 May 2015. http://www.fao.org/docrep/007/ad416e/ad416e05.htm.
- [2] Hexcel Composites, Composite Repair. Publication No. UTC 102, April 1999
- [3] "Fracture Modes." Wikimedia Commons. N.p., 21 Jan. 2008. Web. 12 May 2015.
- http://commons.wikimedia.org/wiki/File:Fracture_modes_v2.svg.
- [4] "Complete Guide to Composites, Part 6." AutoSpeed Articles RSS. N.p., n.d. Web. 19 May 2015.
- http://www.autospeed.com/cms/article.html?&title=Complete-Guide-to-Composites-Part-6&A=108698>.
- [5] ASTM D6671 / D6671M-13, Standard Test Method for Mixed Mode I-Mode II Interlaminar Fracture Toughness of Unidirectional Fiber Reinforced Polymer Matrix Composites, ASTM International, West Conshohocken, PA, 2013

Questions?